## Improvement of response time with an additional bias beam in a BaTiO<sub>3</sub> self-pumped phase-conjugate mirror

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Improvement of the response time of the  $BaTiO_3$  self-pumped phase-conjugate mirror is demonstrated with a simple configuration. It is based on beam amplification in the crystal driven by an additional bias beam.

The photorefractive crystal BaTiO<sub>3</sub> is commonly used as a self-pumped phase-conjugate mirror<sup>1,2</sup> (SPPCM) for its large beam-coupling coefficient. The disadvantage of the SPPCM is its slow response time, which depends mainly on the total intensity of the incident beams.<sup>3</sup> The time response<sup>4</sup> or frequency response<sup>5</sup> in SPPCM's have been described, but there are few reports<sup>6</sup> on improving response time. In this note we report how to improve the response time of BaTiO<sub>3</sub> SPPCM with limited finite laser power. The response time  $\tau$  described here denotes the time required for the generation of a phase-conjugate wave (PCW).

The insets of Fig. 1 show the configuration of the conventional SPPCM and a SPPCM with an additional bias beam. The conventional one is shown in Fig. 1(a). A part of object beam  $I_{11}$  is bent in the direction of the *c* axis and acts as pump beams *a* and *b* in regions 1 and 2, respectively. The beams are reflected at the corner cube of the crystal and play the role of other pump beams *b'* and *a'* at each region. Thus the PCW is generated by internal degenerate four-wave mixing. The energy of the pump beam is supplied from only the object beam. The mechanism has been described in detail in Ref. 3. Response time  $\tau$  of the phase-conjugate mirror, based on the geometry of degenerate four-wave mixing, is evaluated as<sup>3</sup>

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$$\tau = K/I_T,\tag{1}$$

where K is a constant, and  $I_T$  is the total intensity of the incident beam in milliwatts per millimeter squared. To improve the response time, we introduce an additional bias beam, as shown in Fig. 1(b). In this configuration, we use the beam amplification<sup>7</sup> that is based on two-beam coupling,<sup>8</sup> and the process of the generation of PCW is explained as follows. First, bias beam  $I_{21}$  acts as the pump beam, and object beam  $I_{11}$  is amplified by the energy transfer from  $I_{21}$ . Next, self-pumping is generated by the amplified object beam  $I_{11}$  in the same way, as explained in Fig. 1(a). Since the energy of the pump beam is supplied not only from the object beam but also from the bias beam,  $\tau$  is reduced according to Eq. (1). The theory of two-beam coupling has also been explained<sup>7,8</sup>; we do not describe it in detail here.

In practical systems, the intensity of the object beam is limited mainly by the laser power that is used and by amplitude transmittance T of the object. When a plane wave with intensity  $I_{in}$  passes through the object, intensity  $I_A$  of the object beam is given by

$$I_A = TI_{\rm in}.$$
 (2)

On the other hand, if the beam is divided into two by the beam splitter (BS), which has reflection coefficient R, the total intensity  $I_B$  at the crystal is given by

$$I_B = [R + (1 - R)T]I_{\rm in}, \tag{3}$$

where  $RI_{in}$  and  $(1 - R)TI_{in}$  are the intensity that is reflected by the BS and the intensity that is passed through the BS and object, respectively. In our configuration,  $RI_{in}$  is used as the bias beam. Thus, by the use of the BS, the total intensity of the incident

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Fig. 1. Experimental setup. The crystal size is  $5 \text{ mm} \times 5 \text{ mm} \times 5$ mm. The angle  $\theta$  is fixed at 20° and the incident angle of  $I_{21}$  is 90° with respect to the *c* axis.  $I_{12}$  and  $I_{22}$  are the transmitted beams. L's, lenses; BS's, beam splitters; M, mirror. The insets represent the configurations of (a) the conventional SPPCM, (b) the SPPCM with the bias beam.

beam is increased by

$$I_B - I_A = R(1 - T)I_{\rm in}.$$
 (4)

So this method is effective when T is small.

The experimental setup is shown in Fig. 1. An argon-ion laser beam ( $\lambda = 514.5$  nm) is divided into object beam  $I_{11}$  and bias beam  $I_{21}$ , each of which are 2 mm in diameter. The incident angle of  $I_{21}$  was 90° with respect to the *c* axis. The PCW's are  $I_3$  and  $I_4$ , respectively. We measured the response time of ordinary SPPCM for various incident angles  $(\theta's)$ without a bias beam. The power of the incident beam was  $160 \text{ mW/cm}^2$ . The measured results are shown in Fig. 2. The response times were  $\sim 10$  s for  $\theta \leq 20^\circ$ , and we carried out the following experiments at  $\theta \leq 20^{\circ}$ . Figure 3 shows the typical evolutions of PCW's  $I_3$ , and  $I_4$  and the transmitted beam  $I_{12}$  at  $\theta =$ 20°. Both PCW's arose simultaneously at  $t \sim 20$  s. The intensities of  $I_{11}$  and  $I_{21}$  were 10 and 100 mW/cm<sup>2</sup> respectively.  $I_{21}$  was cut off with a shutter at t = 200The evolution of  $I_3$  is shown in Fig. 3(a). It s. fluctuated temporally under the influence of  $I_{21}$  until  $I_{21}$  was cut off with a shutter. When  $I_{21}$  was cut off,  $I_3$  dropped to nearly 0, but arose again immediately because the desired phase grating has been seeded before t reached t = 200 s. Since BaTiO<sub>3</sub> acts as a conventional SPPCM after the interception of the bias beam, the fluctuations in  $I_3$  are not observed. The evolution of  $I_4$  is shown in Fig. 3(b). Since the incident angle was not appropriate for the generation of a PCW, the steady-state output level was smaller



Fig. 2. Response time of the ordinary SPPCM as a function of  $\theta_{\rm c}$  . The power of the incident beam was 160 mW  $[\rm cm^2]$ 

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Fig. 3. Typical revolutions of PCW's  $I_3$  and  $I_4$ , and transmitted beam  $I_{12}$  at  $\theta = 20^\circ$ . The intensities of  $I_{11}$  and  $I_{21}$  were 10 and 100 mW/cm<sup>2</sup>, respectively: (a)  $I_3$ , the phase-conjugated object beam; (b)  $I_4$ , the phase-conjugated bias beam; (c)  $I_{12}$ , the transmitted object beam. The bias beam was intercepted by a shutter at t =200 s.

than  $I_3$ , although the intensity of  $I_{21}$  was ten times as large as  $I_{11}$ . Figure 3(c) shows the evolution of  $I_{12}$ . It fell quickly when  $I_{21}$  was cut off because the energy transferred from  $I_{21}$  was removed. This drop shows that  $I_{11}$  had been amplified by the beam coupling. Response time  $\tau$  and the steady-state intensity of  $I_3$ plotted for  $I_{11}$  are shown in Fig. 4. They were measured for  $\theta = 10^{\circ}$  and  $20^{\circ}$ . Response time  $\tau$  is denoted as the time required for first observing  $I_3$ . The intensity of the bias beam  $I_{21}$  was 50 mW/cm<sup>2</sup>, which was different from that in Fig. 3. Figure 4(a) shows the response time of  $I_3$ . When  $I_{21}$  was not introduced,  $\tau$  increased with the decrease of  $I_{11}$ ; also,  $I_3$  could not be obtained at  $I_{11} = 1$  mW/cm<sup>2</sup>. When  $I_{21}$  was introduced, however,  $\tau$  was mainly dependent



Fig. 4. (a) Response time and (b) steady-state intensities of phase-conjugated object beam  $I_3$  measured for various intensities of the incident object beam  $I_{11}$ .  $\blacktriangle$ ,  $\theta = 10^{\circ}$  and  $\bigcirc$ ,  $\theta = 20^{\circ}$  with bias beam;  $\triangle$ ,  $\theta = 10^{\circ}$  and  $\bigcirc$ ,  $\theta = 20^{\circ}$  without bias beam, at which the intensity of bias beam was fixed to 50 mW/cm<sup>2</sup>. The solid curves are theoretical fits based on Eq. (1).

on  $I_{21}$  with the decrease of  $I_{11}$ . Moreover,  $I_3$  could be obtained even if  $I_{11}$  were 1 mW/cm<sup>2</sup>. The solid curves are calculated with Eq. (1), where K = 20 and  $I_T = I_{11} + I_{21}$ . The dependence on  $\theta$  was almost the same between  $\theta = 10^\circ$  and  $20^\circ$ . So  $\tau$  is inversely proportional to the total intensity of the incident beams and can be improved by the bias beam  $I_{21}$ .

The steady-state intensity of  $I_3$  is shown in Fig. 4(b). It is reduced with the decrease of  $I_{11}$ , whether  $\overline{I}_{21}$  was introduced or not. But the intensity of  $I_3$  obtained with  $I_{21}$  was slightly larger than that without  $I_{21}$ because a part of  $I_{21}$  is transferred to  $I_{11}$  by the beam coupling.  $I_3$  is not amplified much, although the object beam is amplified by the beam coupling, as shown in Fig. 3(c). It is thought that  $I_3$  is distributed by the phase hologram that contributes to the twobeam coupling. The configuration in our experiment is not a complete SPPCM when  $I_{12}$  is not shuttered. But the behavior is the same as a conventional SPPCM except for the fluctuation of  $I_3$ . If one wishes to have a conventional SPPCM, it is necessary only to shut off  $I_{21}$ . An yet  $\tau$  is improved. For example, when  $I_{11} = 10 \text{ mW/cm}^2$ ,  $I_3$  rises at  $t \sim 200 \text{ s}$ without  $I_{21}$ , while it rises completely at t = 100 s with  $I_{21} = 100 \text{ mW/cm}^2$ , as shown in Fig. 4(a). If  $I_{21}$  is shuttered at t = 100 s,  $I_3$  will rise promptly. So  $\tau$ becomes half of that in a conventional SPPCM.

In conclusion, we have demonstrated improvement of the response time of SPPCM by introducing a bias beam. This method can be carried out easily and is useful for obtaining a PCW in a short time from objects that have poor transparency.

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