

# Extension of distance measurement range in a sinusoidal wavelength-scanning interferometer using a liquid-crystal wavelength filter with double feedback control

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The optical path difference (OPD) and amplitude of a sinusoidal wavelength scanning (SWS) are controlled with a double feedback control system in an interferometer, so that a ruler marking every wavelength and a ruler with scales smaller than a wavelength are generated. These two rulers enable us to measure an OPD longer than a wavelength. A liquid-crystal Fabry-Perot interferometer (LC-FPI) is adopted as a wavelength-scanning device, and double sinusoidal phase modulation is incorporated in the SWS interferometer. Because of a high resolution of the LC-FPI, the upper limit of the measurement range can be extended to 280  $\mu\text{m}$  by the use of the phase lock where the amplitude of the SWS is doubled in the feedback control. The ruler marking every wavelength is generated between 80  $\mu\text{m}$  and 280  $\mu\text{m}$ , and distances are measured with a high accuracy of the order of a nanometer in real time. © 2007 Optical Society of America

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## 1. Introduction

Single-wavelength interferometers are limited to measurements of displacement in which a change of the optical path difference (OPD) between two measuring points is smaller than a wavelength. To overcome this limitation, two-wavelength interferometers [1–3] and wavelength-scanning interferometers [4–8] have been developed. Among these interferometers, sinusoidal wavelength-scanning interferometers are the most useful and attractive because sinusoidal wavelength scanning (SWS) can be carried out easily and exactly. Moreover, SWS is unique in that it produces a time-varying interference signal that contains a phase-modulation amplitude  $Z_b$ , due to the SWS besides the conventional phase  $\alpha$ . By processing the interference signal with a computer to calculate the values of  $Z_b$

and  $\alpha$ , and OPD longer than a wavelength can be measured with a high accuracy of the order of a nanometer [8]. On the other hand, operation of the phase lock can be easily carried out with a feedback control system [9] for the interference signals produced by sinusoidal-phase modulation or SWS. By keeping the two values of  $Z_b$  and  $\alpha$  at specified values with double feedback control, a ruler marking every wavelength and a ruler with scales smaller than a wavelength are generated in the SWS interferometer. These two rulers enable us to measure an OPD longer than a wavelength in real time [10].

In this paper characteristics of the SWS interferometer with double feedback control are improved. First a liquid-crystal Fabry-Perot interferometer (LC-FPI) [11] is adopted as a wavelength-scanning device that transmits a portion of the broad light spectrum of a superluminescent diode (SLD). A vibrating slit was used to transmit a portion of the spectrum of a SLD that was generated with a diffractive grating and a

lens in Ref. [10]. Since the slit was vibrated with a speaker to produce the SWS, the resolution in the SWS was about 0.03 nm. This resolution limited the upper value of the measurable OPD to about 100  $\mu\text{m}$ . Since the LC-FPI provides a high resolution in the SWS, it is expected that the upper limit is extended to a few hundreds of microns in OPD. Next, when the LC-FPI is used, frequency  $f_b$  of the SWS becomes smaller. The feedback signal for the phase lock of  $\alpha$  was generated by using a low pass filter whose cutoff frequency was  $f_b/10$  in Ref. [10]. This signal generation makes the frequency bandwidth of the feedback control system very narrow in the use of the LC-FPI. A method using double sinusoidal phase modulation [12] is incorporated in which the frequency bandwidth becomes  $f_b$ . Finally the phase lock of  $Z_b = 2\pi$  is introduced in addition to the phase lock of  $Z_b = \pi$  that was used in Ref. [10]. The new phase lock also extends the upper limit of the measurement range. In experiments it is shown that a ruler marking every wavelength is generated between 80  $\mu\text{m}$  and 280  $\mu\text{m}$  in OPD by using the LC-FPI and the phase lock of  $Z_b = 2\pi$ .

## 2. Interference Signal

Figure 1 shows a schematic diagram of a SWS interferometer with double feedback control. The central wavelength of the SWS light source (SWS-LS) is sinusoidally scanned, and it is expressed by

$$\lambda(t) = \lambda_0 + b \cos(\omega_b t). \quad (1)$$

The output of the SWS-LS is divided into an object beam and a reference beam with a beam splitter (BS). The position of mirror M1 is to be measured. The reference beam is reflected by reference mirror M2, which is displaced by piezoelectric transducer PZT1 and is vibrated by piezoelectric transducer PZT2. Its vibration is a sinusoidal motion of a  $\cos(\omega_c t)$ . The optical path difference (OPD) between the object and reference beam is  $L$ . The interference signal detected with a photodiode (PD) is given by

$$S_D(t) = A + B \cos[Z_c \cos(\omega_c t) + Z_b \cos(\omega_b t) + \alpha], \quad (2)$$

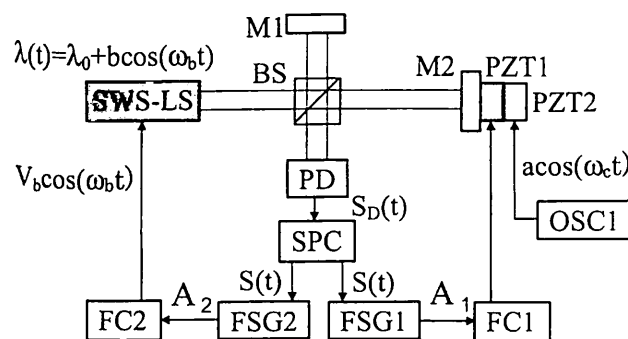


Fig. 1. Schematic diagram of sinusoidal wavelength-scanning interferometer with double feedback control for real-time distance measurement.

where  $A$  and  $B$  are constants, and

$$Z_c = 4\pi a / \lambda_0, \quad (3)$$

$$Z_b = (2\pi b / \lambda_0^2) L, \quad (4)$$

$$\alpha = -(2\pi / \lambda_0) L. \quad (5)$$

Since scanning amplitude  $b$  is very small compared to central wavelength  $\lambda_0$ ,  $\lambda(t)$  is approximated as  $\lambda_0$  in Eq. (3), and an approximation of  $1/\lambda(t) = (1/\lambda_0) - [b \cos(\omega_b t) / \lambda_0^2]$  is used to derive Eqs. (4) and (5). Putting  $\phi(t) = Z_b \cos \omega_b t + \alpha$ , Eq. (2) is expressed as

$$S_D(t) = A + B \cos \phi(t) [J_0(Z_c) - 2J_2(Z_c) \cos 2\omega_c t + \dots] - B \sin \phi(t) [2J_1(Z_c) \cos \omega_c t + 2J_3(Z_c) \cos 3\omega_c t + \dots], \quad (6)$$

where  $J_n$  is the  $n$ th-order Bessel function.

$S_D(t)$  is multiplied by  $\cos(\omega_c t)$ , and we use a low pass filter in signal processing circuits SPC to extract frequency components around  $\omega_c$  in the condition of  $\omega_b < \omega_c$  from signal  $S_D(t)$ . We obtain the following interference signal to be used for double feedback control:

$$S(t) = C \sin[Z_b \cos(\omega_b t) + \alpha], \quad (7)$$

where  $C = -2BJ_1(Z_c)$ . The amplitude  $a$  of the vibration in Eq. (3) is adjusted so that  $J_1(Z_c)$  has a maximum value.

## 3. Measurement Principle

First, it is explained how to measure a fractional value of OPD  $L$  with a feedback control. Sampling  $S(t)$  at  $\cos \omega_b t = 0$  with sample holders in feedback signal generator FSG1 produces a feedback signal

$$A_1 = C \sin \alpha, \quad (8)$$

whose frequency bandwidth is allowed to be  $\omega_b/2\pi$ . Feedback controller FC1 produces voltage  $V_\alpha$  applied to the PZT1. The feedback system controls the position of reference mirror M<sub>R</sub> or the OPD so that the feedback signal  $A_1$  becomes zero. A change in the OPD caused by this feedback control is illustrated in Fig. 2. First the OPD is  $L$  and the position of signal  $A_1$  is at point  $Q$ . The position of signal  $A_1$  is moved to a stable point  $P$  by the feedback control. Phase  $\alpha$  becomes  $2m\pi$ , where  $m$  is an integer. The OPD at the stable point of the feedback control is given by

$$L_z = L - L_\alpha = m\lambda_0. \quad (9)$$

$L_\alpha$  is a fractional value of OPD  $L$  to be measured. The range of  $L_\alpha$  is approximately between  $-\lambda_0/2$  and  $\lambda_0/2$ . When a change  $\Delta V_\alpha$  is detected in  $V_\alpha$  after an OPD  $L$  is given,  $L_\alpha = \beta \Delta V_\alpha$  is obtained. Constant  $\beta$  means a change in OPD  $L$  for a change of 1 voltage in  $V_\alpha$ . The

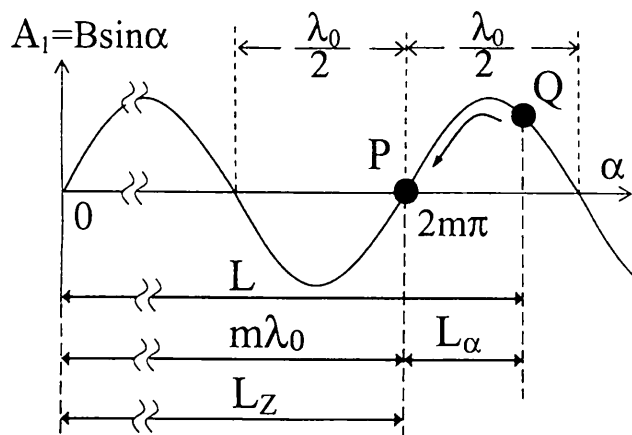


Fig. 2. Change in the OPD by feedback control, which keeps phase  $\alpha$  at  $2m\pi$ .

measurement accuracy of  $L_a$  is of the order of nanometers.

Next, it is explained how to measure an integer multiple of the wavelength in the OPD  $L$ . Since the phase  $\alpha$  is kept at  $2m\pi$  by feedback control, the interference signal is

$$S(t) = C \sin[Z_b \cos(\omega_b t)], \quad (10)$$

where

$$Z_b = (2\pi b / \lambda_0^2) L_z. \quad (11)$$

Signal  $S(t)$  is sampled with sample holders when  $\cos \omega_b t = 1$  and  $\cos \omega_b t = -1$  so that signals  $S_1 = B \sin Z_b$  and  $S_{-1} = -B \sin Z_b$  are obtained. From these signals a feedback signal

$$A_2 = S_{-1} - S_1 = -2B \sin Z_b \quad (12)$$

is generated in feedback signal generator FSG2. Feedback controller FC2 produces amplitude  $V_b$  of the signal applied to a wavelength-tunable filter contained in the SWS-LS. The feedback system controls the amplitude  $V_b$  or the amplitude  $b$  of the wavelength scanning so that the signal  $A_2$  becomes zero. The feedback signal given by Eq. (12) makes modulation amplitude  $Z_b$  equal to  $p\pi$ , where  $p$  is equal to 1 or 3 as shown in Fig. 3(a). When the value of  $Z_b$  is less than  $2\pi$ , the phase lock of  $Z_b = \pi$  is produced. When the sign of the feedback signal  $A_2$  given by Eq. (12) is inverted, the phase lock of  $Z_b = p\pi$  is produced, where  $p$  is equal to 2 or 4 as shown in Fig. 3(b).

When  $Z_b = p\pi$  is satisfied by the phase lock, Eqs. (9) and (11) lead to

$$b = p\lambda_0^2 / 2L_z = p\lambda_0 / 2m. \quad (13)$$

The values of  $b$  are discrete, corresponding to the values of  $m$ . Since amplitude  $b$  is proportional to amplitude  $V_b$  with a form of  $b = D_1 V_b + D_0$ , the values of  $V_b$  are also discrete. These discrete values of the

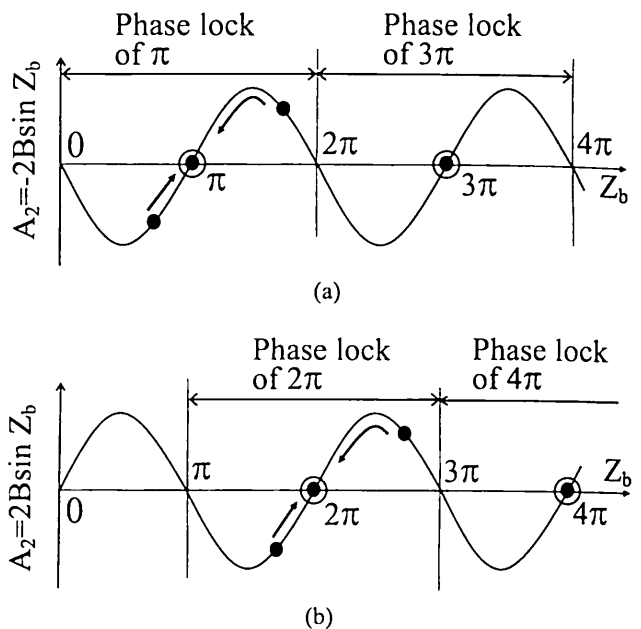


Fig. 3. Regions of  $Z_b$  where the phase lock of  $Z_b = p\pi$  occurs when the feedback signal is (a)  $A_2 = -2B \sin Z_b$  and (b)  $A_2 = 2B \sin Z_b$ .

amplitude  $V_b$  at which  $Z_b$  is equal to  $p\pi$  are referred to as stable points of  $V_b$ . Since the stable points of  $V_b$  correspond to the values of  $m$ , the stable points are regarded as a ruler marking every wavelength. On the other hand, the voltage  $V_a$  is regarded as a ruler with scales smaller than a wavelength. The calibration of the ruler produced by the stable points of  $V_b$  can be made automatically by double feedback control by changing the OPD at intervals of approximately a wavelength.

When the relation of  $b = D_1 V_b + D_0$  is known beforehand, the value of  $b$  is obtained from the value of  $V_b$  detected at the stable point, and a measured value of  $L_z$  is calculated by the relation of  $L_z = p\lambda_0^2 / 2b$ . Since  $L_z$  is given by Eq. (9), the following value is calculated by using the measured value of  $L_z$ :

$$m_c = L_z / \lambda_0. \quad (14)$$

Integer  $m$  can be decided by rounding off the value of  $m_c$  to an integer if a measurement error of  $L_z$  is smaller than  $\lambda_0 / 2$ . Therefore, the OPD is obtained as follows:

$$L = m\lambda_0 + L_a. \quad (15)$$

#### 4. Extension of Measurement Range

When a stable point of  $V_b$  at  $L_z$  moves to the adjacent stable point of  $V_b + \Delta V_b$  due to increasing the OPD by about a wavelength, the following change  $\Delta b$  in the wavelength-scanning amplitude  $b$  occurs:

$$\Delta b = -(p\lambda_0^3 / 2L_z^2). \quad (16)$$

The measurement range of the OPD is estimated theoretically from Eqs. (13) and (16) as follows: The

lower and upper limits of the measurable OPD depend on a maximum value and the resolution of the wavelength-scanning amplitude, respectively. Thus characteristics of the wavelength-tunable filter used in the SWS-LS are very important for determination of the measurement range.

In a case of  $p = 1$ ,  $L_z = 100 \mu\text{m}$ , and  $\lambda_0 = 840 \text{ nm}$ , Eqs. (13) and (16) lead to  $b = 3.5 \text{ nm}$  and  $\Delta b = 0.03 \text{ nm}$ . The change  $\Delta V_b$  in a stable point of  $V_b$  corresponding to the change  $\Delta b = 0.03 \text{ nm}$  is roughly equal to  $V_b \times 10^{-3}$  in the relation of  $b = D_1 V_b + D_0$ . Fluctuation of the value of  $V_b$  in experiments must be so small that the value of  $V_b$  does not drift to the value of  $V_b + \Delta V_b$ . It is desirable that a value of  $\Delta V_b$  or  $\Delta b$  is increased to clearly distinguish between the two different values of the adjacent stable points. To meet this requirement, the phase lock of  $Z_b = p\pi$  ( $p = 2, 3, \dots$ ) is adopted instead of the phase lock of  $Z_b = \pi$ . When the value of  $\Delta b$  is enlarged  $p$  times by adopting the phase lock of  $Z_b = p\pi$ , an upper limit of the measurable OPD can be increased by  $p^{1/2}$ .

## 5. Experimental Setup

The SWS interferometer shown in Fig. 1 has been constructed. The schematic illustration of the SWS-LS is shown in Fig. 4. A SLD was used as a broadband light source whose central wavelength  $\lambda_0$  and spectral bandwidth were 844.26 nm and 20 nm, respectively. The output from the SLD was collimated with lens L1, and the diameter of the collimated beam was about 3 mm. A liquid-crystal Fabry–Perot interferometer (LC-FPI) was used as a wavelength-tunable filter. The LC-FPI transmits a very narrow spectrum whose bandwidth is 1.4 nm and whose central wavelength is tuned by a voltage applied to the LC-FPI. The tuned wavelength is varied from 820 nm to 860 nm for static tuning. The LC-FPI was placed in a focal plane of lens 2 whose focal length was 50 mm. A voltage of  $V_b \cos(\omega_b t)$  was applied to the LC-FPI to produce a sinusoidal wavelength scanning of  $\lambda(t) = \lambda_0 + b \cos(\omega_b t)$ . The frequency of  $\omega_b/2\pi$  was 120 Hz. The light transmitted by the LC-FPI was collimated with lens L3 and was split by a polarizer beam splitter (PBS) into two light beams. One of them was wavelength scanned and was used as the output of the SWS-LS for the interferometer.

Sinusoidal vibration frequency  $\omega_c/2\pi$  of the reference mirror M2 was  $64 \times (\omega_b/2\pi) = 7.68 \text{ kHz}$ . The vibration amplitude was adjusted so that  $J_1(Z_c)$  became a maximum value. Change  $L_a$  in the OPD pro-

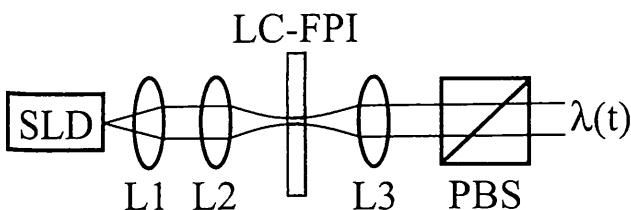


Fig. 4. Schematic illustration of the sinusoidal wavelength-scanning light source (SWS-LS) using a liquid-crystal Fabry–Perot interferometer (LC-FPI).

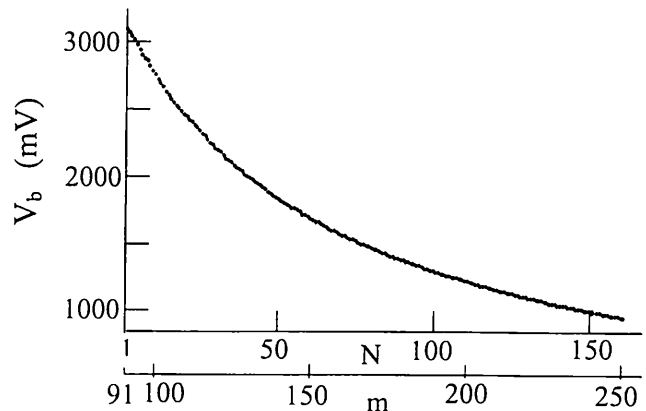


Fig. 5. Stable points of  $V_b$  obtained at the phase lock of  $Z_b = \pi$ .  $N$  is the number of the stable points. The stable point is assigned to the number  $m$  in which  $L_z = m\lambda_0$ .

vided by the displacement of the reference mirror was expressed by  $L_a = \beta \Delta V_a$ , where  $\beta = 83.37 \text{ nm/V}$ . Mirror M1 fixed on a stage was used as an object.

## 6. Experimental Results

When changes in OPD  $L$  were made at intervals of one wavelength by utilizing the feedback control of OPD at a fixed value of  $V_b$ , values of  $Z_b$  were calculated from the interference signal given by Eq. (2) with a computer by the method of double sinusoidal phase modulating interferometry described in Ref. [12]. Three values of  $b$  at  $V_b = 1.0 \text{ V}$ ,  $1.5 \text{ V}$ , and  $2.0 \text{ V}$  were obtained from the values of  $Z_b$  calculated for the changes in  $L$ , and finally the relation of  $b$  [nm] =  $1.47V_b$  [V] + 0.31 was obtained.

Displacements were given to the object with a micrometer to change the OPD. By increasing the OPD at intervals of about one wavelength, a stable point of  $V_b$  could be moved to the next point automatically. 160 stable points of  $V_b$  were obtained at the phase lock of  $Z_b = \pi$  as shown in Fig. 5, whose horizontal axis is the number  $N$  of the stable point. These values of  $V_b$  at the stable points were converted into values of  $b$  with the relation between  $b$  and  $V_b$  to obtain measured values of  $L_z = \lambda_0^2/2b$ . Values of  $m_c$  were calculated from the measured values of  $L_z$  with Eq. (14). Since the absolute value of the difference between the value of  $m_c$  and an integer of its round

Table 1. Measured Values at the Phase Lock of  $Z_b = \pi$

$V_b$ [mV]	$b$ [nm]	$L_z$ [ $\mu\text{m}$ ]	$m_c$	$m$
2217	3.57	99.842	118.3	118
2198	3.54	100.630	119.2	119
2179	3.51	101.430	120.1	120
1412	2.39	149.367	176.9	177
1400	2.37	150.480	178.3	178
1391	2.36	151.326	179.3	179
980	1.751	203.551	241.1	241
976	1.745	204.237	241.9	242
972	1.739	204.928	242.7	243

Table 2. Measured Values at the Phase Lock of  $Z_b = 2\pi$

$V_b$ [mV]	$b$ [nm]	$L_Z$ [ $\mu\text{m}$ ]	$m_c$	$m$
2175	3.51	203.200	240.7	241
2165	3.49	204.055	241.7	242
2154	3.48	205.005	242.8	243
1523	2.55	279.610	331.2	331
1518	2.54	280.419	332.2	332
1513	2.53	281.232	333.1	333

number was less than 0.5 in the region of  $N = 20-140$ , values of integer  $m$  and the relation of  $m = N + 90$  could be determined as shown in Fig. 5. Table 1 shows the values of  $b$ ,  $L_Z$ ,  $m_c$ , and  $m$  for some stable points in the different regions around  $L_Z = 100 \mu\text{m}$ ,  $150 \mu\text{m}$ , and  $200 \mu\text{m}$ . Since the magnitude of the fluctuations in values of the stable points with time was close to the value of  $\Delta b$  around  $L_Z + 200 \mu\text{m}$ , about  $200 \mu\text{m}$  was the upper limit of the measurable OPD at the phase lock of  $Z_b = \pi$ . It is estimated that the resolution of the wavelength scanning is higher than the value of  $\Delta b$  given by Eq. (16) at  $L_Z = 204 \mu\text{m}$ , that is,  $0.007 \text{ nm}$ .

The sign of the feedback signal  $A_2$  was inverted at the stable point of  $V_b = 980 \text{ mV}$  shown in Table 1 for the phase lock of  $Z_b = 2\pi$  to start. The values of the stable points around  $L_Z = 200 \mu\text{m}$  at the phase lock of  $Z_b = \pi$  shown in Table 1 were changed to the values shown at Table 2. The same values of  $m$  were obtained, although the values of  $L_Z$  or  $m_c$  changed a little. The results made it clear that using the phase lock of  $Z_b = 2\pi$  enlarges the values of  $\Delta V_b$  about two times. Stable points for up to  $L_Z = 280 \mu\text{m}$  could be obtained as shown at Table 2.

Finally, displacement  $D$  of mirror M1 was measured that was given with the micrometer. Values of  $V_b$  and  $\Delta V_a$  are detected as shown at Table 3, where the phase lock of  $Z_b = \pi$  was switched to the phase lock of  $Z_b = 2\pi$  at  $2D = 100 \mu\text{m}$ . The value of  $m$  was decided by the relation between the stable points of  $V_b$  and the values of  $m$ . The value of  $L_a$  was calculated with  $L_a = 83.37\Delta V_a$ .  $\Delta L$  was the difference between the two values of OPD measured successively. There were differences between  $2D$  and  $\Delta L$  because the displacement given by the micrometer was not so accu-

Table 3. Results of Distance Measurement

$2D$	$V_b$ [mV]	$m$	$\Delta V_a$ [V]	$L_a$ [ $\mu\text{m}$ ]	$L$ [ $\mu\text{m}$ ]	$\Delta L$
0	2302	114	3.9	0.325	95.564	
50	1437	174	-4.3	-0.358	146.533	49.969
100	1021	233	0.4	0.033	196.733	50.200
100	2251	233	0.4	0.033	196.733	
150	1748	293	3.4	0.283	247.635	50.902
180	1550	326	4.9	0.409	275.619	27.984

rate. Since the measurement error in  $\Delta V_a$  was estimated to be less than  $0.05 \text{ V}$ , the measurement error in  $L_a$  was less than  $4 \text{ nm}$ .

## 7. Conclusion

The liquid-crystal Fabry-Perot interferometer (LC-FPI) was adopted as a wavelength-scanning device in the SWS interferometer with double feedback control. By incorporating double sinusoidal phase modulation, a better interference signal was obtained from which the feedback signal with frequency bandwidth equal to the frequency of the SWS could be generated. Because of the high resolution of the LC-FPI, the upper limit of the measurement range was obtained at  $200 \mu\text{m}$  at the phase lock of  $Z_b = \pi$ . Moreover, the phase lock of  $Z_b = 2\pi$  was used instead of  $Z_b = \pi$  in the region longer than  $200 \mu\text{m}$ , so that the upper limit of the measurement range became  $280 \mu\text{m}$ . The measurement range was from  $80 \mu\text{m}$  to  $290 \mu\text{m}$  with the measurement error less than  $4 \text{ nm}$ .

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